

Week 12

Nov 21, 2020

2020 A. Adv. Calc. II

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Let  $\vec{r}: D \rightarrow S$  be a parametrization of  $S$ . The tangent space at  $\vec{r}(u,v)$  is spanned by the 2 vectors  $\vec{r}_u$  and  $\vec{r}_v$ . The cross product  $\vec{r}_u \times \vec{r}_v$  provides a vector sub. lying

$$\vec{r}_u \times \vec{r}_v \cdot \vec{r}_u = 0, \quad \vec{r}_u \times \vec{r}_v \cdot \vec{r}_v = 0,$$

hence  $\vec{r}_u \times \vec{r}_v$  lies on the normal direction of  $S$  at  $\vec{r}(u,v)$ .

( $\vec{r}_u \times \vec{r}_v \neq \vec{0}$  as  $\vec{r}$  is assumed to be regular.)

A choice of a continuous unit normal v.f.  $\hat{n}$  is called an orientation of  $S$ . A surface with a given unit normal v.f. is called an oriented surface. Hence

$$\hat{n} = \frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|}, \quad \text{or} \quad \hat{n} = -\frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|}.$$

Let  $S$  be an oriented surface and  $\vec{F}$  a continuous v.f. on  $S$ , the flux of  $\vec{F}$  through  $S$  (or across  $S$ ) is

$$\iint_S \vec{F} \cdot \hat{n} \, d\sigma. \quad (1)$$

We have

$$\begin{aligned} \iint_S \vec{F} \cdot \hat{n} \, d\sigma &= \iint_S \vec{F} \cdot \left( \pm \frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|} \right) d\sigma \\ &= \iint_D \vec{F}(\vec{r}(u,v)) \cdot \left( \pm \frac{\vec{r}_u \times \vec{r}_v}{|\vec{r}_u \times \vec{r}_v|} \right) dA(u,v) \\ &= \iint_D \vec{F}(\vec{r}(u,v)) \cdot \left( \pm \vec{r}_u \times \vec{r}_v \right) dA(u,v) \quad (2) \end{aligned}$$

( $\pm$  means to choose  $\hat{n}$  s.t.  $= \pm$ )

① and ② can be used to find the flux.

e.g. Find the flux of  $\vec{F} = (yz, x, -z^2)$  through the parabolic cylinder  $y = x^2, 0 \leq x \leq 1, 0 \leq z \leq 4$ , in the indicated direction (see text for the picture).

$S$  is a graph over  $[0, 1] \times [0, 4] \sim$  the  $xz$ -plane.

$$(x, z) \mapsto (x, x^2, z)$$

$$\vec{r}_x \times \vec{r}_z = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 1 & 2x & 0 \\ 0 & 0 & 1 \end{vmatrix} = (2x, -1, 0)$$

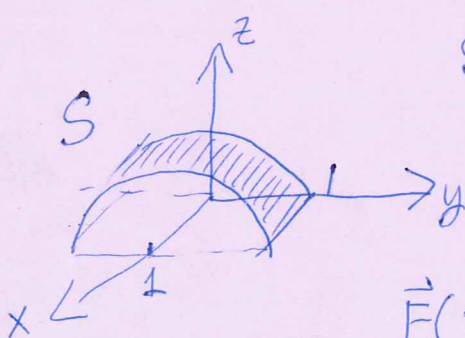
We require  $\hat{n}$  points to the  $x$  direction, so this is the correct choice.

$$\vec{F}(\vec{r}(x, z)) = (x^2z, x, -z^2)$$

$$\vec{F}(\vec{r}(x, z)) \cdot \vec{r}_x \times \vec{r}_z = (x^2z, x, -z^2) \cdot (2x, -1, 0) = 2x^3z - x.$$

$$\begin{aligned} \therefore \text{flux} &= \iint_S \vec{F} \cdot \hat{n} \, d\sigma = \iint_{[0, 1] \times [0, 4]} \vec{F}(\vec{r}(x, z)) \cdot \vec{r}_x \times \vec{r}_z \, dA(x, z) \quad (\text{see } \textcircled{2}) \\ &= \int_0^1 \int_0^4 (2x^3z - x) \, dz \, dx \\ &= 2. \# \end{aligned}$$

e.g. Find the flux of  $\vec{F} = yz\hat{j} + z^2\hat{k}$  outward through the surface  $S$  cut from  $y + z^2 = 1, z \geq 0$ , by the plane  $x = 0, x = 1$ .



$S$  is a graph over  $[0, 1] \times [-1, 1] \sim xy$ -plane

$$(x, y) \mapsto (x, y, \sqrt{1-y^2})$$

$$\vec{r}_x \times \vec{r}_y = (0, \frac{y}{\sqrt{1-y^2}}, 1), \text{ it is in the right orientation}$$

$$\vec{F}(\vec{r}(x, y)) = y\sqrt{1-y^2}\hat{j} + (1-y^2)\hat{k}$$

$$\therefore \text{flux} = \iint_S \vec{F} \cdot \hat{n} \, d\sigma = \iint_{[0, 1] \times [-1, 1]} (y\sqrt{1-y^2}\hat{j} + (1-y^2)\hat{k}) \cdot \left(\frac{y}{\sqrt{1-y^2}}\hat{j} + \hat{k}\right) \, dA(x, y) \quad (\text{by } \textcircled{2})$$

$$= \int_0^1 \int_{-1}^1 1 \, dy \, dx = 2.$$

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(There is no need to use implicit surface as in Text.)

(Cont'd)

Stokes' theorem Let  $S$  be a piecewise smooth oriented surface whose boundary is a piecewise smooth simple closed curve  $C$ . For a smooth v.f.  $\vec{F}$  defined in some open region containing  $S$ ,

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_S \nabla \times \vec{F} \cdot \hat{n} \, d\sigma.$$

Here  $\hat{n}$  is the chosen normal for  $S$ , and the orientation of  $C$  is anticlockwise w.r.t.  $\hat{n}$ , and  $\nabla \times \vec{F}$  is the curl of  $\vec{F}$ :

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ M & N & P \end{vmatrix}$$

$$= (P_y - N_z)\hat{i} - (P_x - M_z)\hat{j} + (N_x - M_y)\hat{k}.$$

e.g. Verify Stokes' theorem for  $x^2 + y^2 + z^2 = 9, z \geq 0$ , outward pointing normal, and its boundary  $C, x^2 + y^2 = 9$ , for  $\vec{F} = y\hat{i} - x\hat{j}$ .

$$\text{Here } \hat{n} = \frac{(x, y, z)}{\sqrt{x^2 + y^2 + z^2}} \text{ (for any sphere at } (0, 0, 0))$$

$$= \frac{1}{3}(x, y, z)$$

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ y & -x & 0 \end{vmatrix} = (0, 0, -2) = -2\hat{k}$$

$$\nabla \times \vec{F} \cdot \hat{n} = \frac{1}{3}(x, y, z) \cdot (-2\hat{k}) = -\frac{2}{3}z$$

Use  $(x, y) \mapsto (x, y, \sqrt{9-x^2-y^2})$ ,  $(x, y) \in D_3$  to parametrize  $S$

$$\begin{aligned} d\sigma &= \sqrt{1 + f_x^2 + f_y^2} dA \\ &= \sqrt{1 + \frac{x^2}{9-x^2-y^2} + \frac{y^2}{9-x^2-y^2}} dA \\ &= \sqrt{\frac{9}{9-x^2-y^2}} dA \end{aligned}$$

$$\iint_S \nabla \times \vec{F} \cdot \hat{n} d\sigma = \iint_{D_3} -\frac{2}{3} \sqrt{9-x^2-y^2} \frac{3}{\sqrt{9-x^2-y^2}} dA = -2 \iint_{D_3} dA = -18\pi.$$

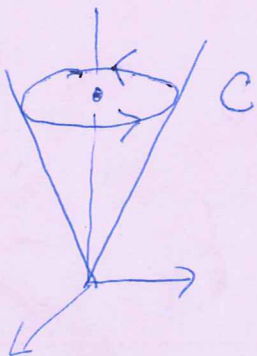
On the other hand, the correct orientation of  $C$  is

$$\vec{r}(\theta) : \theta \mapsto (3\cos\theta, 3\sin\theta, 0), \quad \theta \in [0, 2\pi]$$

$$\vec{r}'(\theta) = (-3\sin\theta, 3\cos\theta, 0)$$

$$\begin{aligned} \oint_C \vec{F} \cdot d\vec{r} &= \int_0^{2\pi} \vec{F}(\vec{r}(\theta)) \cdot (-3\sin\theta, 3\cos\theta, 0) d\theta \\ &= \int_0^{2\pi} (3\sin\theta, -3\cos\theta, 0) \cdot (-3\sin\theta, 3\cos\theta, 0) d\theta \\ &= -18\pi. \# \end{aligned}$$

e.g. Calculate the circulation around the bounding circle  $C$  of the v.f.  $(x^2-y)\hat{i} + 4z\hat{j} + x^2\hat{k}$  where  $C$  is the intersection of  $z=2$  and  $z=\sqrt{x^2+y^2}$ , anticlockwise as viewed from above.



Now  $C$  is the boundary of 2 surfaces.  
 $S_1$ , the cone  $z = \sqrt{x^2+y^2}$ ,  
 $S_2$ , the flat disk.  
 Apparently, better to work on  $S_2$ .

Take the parametrization

$$(x, y) \mapsto (x, y, z), \quad (x, y) \in D_2$$

for  $S_2$ .  $\vec{r}_x \times \vec{r}_y = (0, 0, 1)$ . The orientation is compatible with the anticlockwise direction of  $C$ .

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ x^2 - y & 4z & x^2 \end{vmatrix} = -4\hat{i} - 2x\hat{j} + \hat{k}$$

$$\iint_{S_2} \nabla \times \vec{F} \cdot \hat{n} \, d\sigma = \iint_{D_2} \nabla \times \vec{F} \cdot \vec{r}_x \times \vec{r}_y \, dA$$

$$= \iint_{D_2} (-4\hat{i} - 2x\hat{j} + \hat{k}) \cdot \hat{k} \, dA$$

$$= \iint_{D_2} dA$$

$$= 4\pi$$

By Stokes', the circulation is

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_{S_2} \nabla \times \vec{F} \cdot \hat{n} \, d\sigma = 4\pi \quad \#$$

e.g. Let  $S$  be the portion of the hyperbolic paraboloid  $z = y^2 - x^2$  inside the cylinder  $x^2 + y^2 = 1$ , with normal pointing upward. Find the circulation of  $\vec{F} = y\hat{i} - x\hat{j} + x^2\hat{k}$  around its boundary curve (in anticlockwise viewed from above).

Use the parametrization

$$(x, y) \mapsto (x, y, y^2 - x^2)$$

$$\vec{r}_x \times \vec{r}_y = (-2x, 2y, 1) \quad (\text{the chosen orientation})$$

$$\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ y & -x & x^2 \end{vmatrix} = -2x\hat{j} - 2\hat{k}$$

$$\nabla \times \vec{F} \cdot \vec{r}_x \times \vec{r}_y = (-2x\hat{j} - 2\hat{k}) \cdot (-2x\hat{i} + 2y\hat{j} + \hat{k})$$

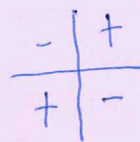
$$= -4xy - 2$$

$$\iint_S \nabla \times \vec{F} \cdot \hat{n} d\sigma = \iint_{D_1} (-4xy - 2) dA$$

$$= -2 \iint_{D_1} dA$$

$$= -2\pi \#$$

(  $\iint_{D_1} xy dA = 0$  due to symmetry )



Return to Stokes' theorem.

Some Remarks

① Reduction to Green's theorem.

Regard  $D$  as a flat surface  $S_0$ .

$$(x, y) \leftrightarrow (x, y, 0)$$

Regard  $\vec{F} = M(x, y)\hat{i} + N(x, y)\hat{j}$  as

$$\vec{F}_1 = M(x, y)\hat{i} + N(x, y)\hat{j} + 0\hat{k} \text{ in space.}$$

Choose  $\hat{n} = (0, 0, 1)$  for  $S_0$  and then  $C_1$ , the boundary of  $S_0$ , will be in anticlockwise direction.

$$C_0 \leftrightarrow C_1$$

$$(x(t), y(t)) \quad (x(t), y(t), 0)$$

Stokes' thm applies to  $S_0$  and  $C_1$ :

$$\nabla \times \vec{F}_1 = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \\ M & N & 0 \end{vmatrix} = (N_x - M_y)\hat{k}$$

$$\nabla \times \vec{F}_1 \cdot \hat{n} = (N_x - M_y)\hat{k} \cdot \hat{k} = N_x - M_y$$

$$\begin{aligned} \therefore \iint_S \nabla_x \vec{F}_1 \cdot \hat{n} d\sigma &= \iint_S (N_x - M_y) d\sigma & d\sigma &= \sqrt{1 + f_x'^2 + f_y'^2} dA \\ &= \iint_D (N_x - M_y) dA & &= \sqrt{1 + 0 + 0} dA \\ & & &= dA \end{aligned} \quad (3)$$

On the other hand,

$$\begin{aligned} \oint_{C_1} \vec{F} \cdot d\vec{r} &= \int_a^b (M(x(t), y(t)) \hat{i} + N(x(t), y(t)) \hat{j} + 0 \hat{k}) \cdot (x' \hat{i} + y' \hat{j} + 0 \hat{k}) dt \\ &= \int_a^b (Mx' + Ny') dt \\ &= \oint_C M dx + N dy. \quad (4) \end{aligned}$$

(3) + (4)

$$\iint_S \nabla_x \vec{F}_1 \cdot \hat{n} d\sigma = \oint_{C_1} \vec{F} \cdot d\vec{r} \Rightarrow \iint_D (N_x - M_y) dA = \oint_C M dx + N dy. \quad \#$$